

"Review Article"

Hysteresis: Phenomenon and Modeling in Soil- Water Relationship

A. IZADY^{1*}, B. GHAHRAMAN^{1**} AND K. DAVARI^{1*}

¹Department of Water Engineering, College of Agriculture, Ferdowsi University of Mashhad, Mashhad, I.R. Iran

ABSTRACT-Hysteresis has been widely recognized in the soil water relationship. In this paper, a detailed review of hysteresis was performed in relation to its models. So far, different models have been suggested to describe hysteresis in the water retention curve (WRC) that could be categorized into two main groups: *conceptual* and *empirical* models. The models in the first group are based on the domain theory of capillary hysteresis and those in the second group rely on the analysis of observed WRC shape and properties. *Conceptual* models include the *independent* and *dependent domain theories* and the *Parlange's model*, while *empirical* models consist of the *interpolation, linear, Slope and Scaling – down* models. Different results of studies carried out by several researchers showed that the *Parlange* model, that uses the concept of rational extrapolation, was the best model to predict hysteresis of the WRC.

Keywords: Conceptual Model, Empirical Model, Hysteresis, Parlange Model

INTRODUCTION

The description and prediction of water flow through unsaturated soils imply an understanding of unsaturated soil properties. The main unsaturated soil properties used in engineering calculations are the relationships between suction (or water pressure), ψ , (cm of water or kPa) and volumetric water content, θ , (cm^3/cm^3) as well as that between suction and hydraulic conductivity, K . These two relationships comprise the *water retention curve* (WRC) and permeability function, respectively. Due to the complex nature of the liquid-phase configuration in an unsaturated porous medium, the relationship between water pressure and water content is not unique and presents hysteresis effects (e.g. 14, 43, 52 and 5). As shown in Figure 1, a soil typically shows a volumetric water content that is less for a wetting process (such as infiltration) than for a drying process (such as evaporation or drainage) at a given water pressure.

* PhD Student, Professor, Associate Professor and Assistant Professor, respectively

** Corresponding Author

The hysteresis effect can be attributed to 4 main causes (e.g. 18 and 37): a) geometric nonuniformity of individual pores, resulting from the so called “Ink Bottle” effect, b) different spatial connectivity of pores during drying or wetting processes, c) variation in the liquid-solid contact angle, where the contact angle and the radius of curvature are greater in the case of an advancing meniscus than the case of a receding one. A given water content will, therefore, tend to exhibit greater suction in desorption than sorption, and d) air entrapment, which further reduces the water content of newly wetted soil. Failure to attain true equilibrium (though not, strictly speaking, true hysteresis) can accentuate the hysteresis effect.

The two complete characteristic curves, from saturation to dryness and vice versa, are the *main branches* of the hysteretic soil moisture characteristics. When a partially wetted soil commences to drain, or when a partially desorbed soil is rewetted, the relation of suction to moisture content follows a number of intermediate curves as it moves from one main branch to the other. Such intermediate spurs are called *scanning curves*.

In the past, hysteresis was generally disregarded in the practice of soil physics. This may be justifiable in the treatment of processes involving monotonic wetting (e.g., infiltration) or monotonic drying (e.g., evaporation). Nevertheless, hysteresis may be important in cases of composite processes where wetting and drying occur simultaneously or sequentially in various parts of the soil profile (e.g., redistribution). Two soil layers of identical texture and structure may be at equilibrium with each other (i.e., at identical energy states) and yet may differ in wetness if their sorbing-desorbing histories have been different. Furthermore, hysteresis can affect dynamic, as well as static properties of the soil (i.e., hydraulic conductivity and flow phenomena).

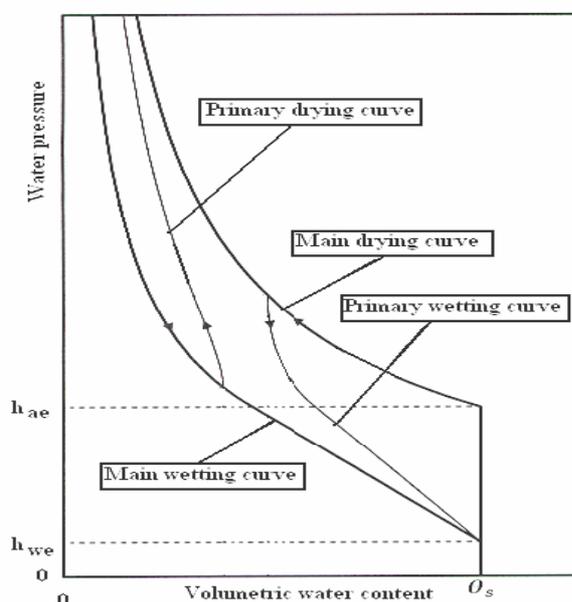


Fig. 1. Schematic representation of water retention curves with hysteresis effects

Because of the important effects of hysteresis on most soils, especially coarse-textured soils (18), different models have been developed to describe different hysteresis curves (main, primary and secondary curves) of the WRC over the last 40

years. This paper presents a brief explanation of the models developed so far. A comparison of these models is then presented for assessment.

HYSTERESIS MODELS

The different approaches that have been used to describe hysteresis in WRC can be categorized into two main groups: *conceptual* and *empirical* models. The first group is based on the domain theory of capillary hysteresis. This theory assigns soil water to domains according to a distribution function $f(\psi_d, \psi_w)$, where the subscripts stand for drying and wetting, respectively. Knowledge of this distribution function allows for the determination of the moisture content by integrating the filled domains after any series of wetting or drying. Empirical models rely on the analysis of observed WRC shape and properties.

Another possible classification of the model is based on the model's parameter identification requirements. Most of these models present the relationship between different WRC curves. A model that describes an arbitrary curve as a function of n other curves, can be referred to as an "*n-branch*" model.

CONCEPTUAL MODELS

Independent Domain Theory

The use of the independent domain theory for water content-pressure head hysteresis as formulated by Everett et al. (10 and 11) is dependent on two assumptions: first, that the pore space is made up of pores or domains, each defined by two pressure head values, one where the pore drains and one where it fills precipitously. The draining and filling of each pore takes place at its defining pressure head values independent of the remaining pores in the system. Second, the water volume difference between the drained and filled states of each pore is independent of the pressure head. It should be noted that the term domain is used here to refer to a group of molecules, or some elements of the system, which can exist in either of the two states (11). If the main branch curve and a set of primary scanning curves (e.g., redrying) are used to define the pore configuration in terms of the domain model, then the other set of primary curves (rewetting) or any other wetting and drying curve patterns can be predicted from the theory.

Poulovassilis (43) was the first to apply the theory to predict redry from rewet scanning curves. Using a disc of sintered glass beads Poulovassilis got encouraging agreement between these predictions and his experimentally-measured data.

Using a dynamic technique, Topp and Miller (52) determined the hysteresis behavior of two artificial porous bodies prepared from glass beads, and compared their experimental data with the prediction of the independent domain hypothesis. One of their porous bodies consisted of uniform glass beads (monodispersed porous body) and the other, was comprised of aggregates made of glass beads. In both bodies the particles were loose and presented a rather narrow range of pore sizes, especially in the case of the monodispersed system. The results showed that predictions were in very poor agreement with the experimental data.

The discrepancy between these results and those of Poulouvassilis (43) could perhaps be due merely to differences in the employed media. In this study, the theory fits the aggregated sample somewhat better than it does for the monodispersed sample. This may indicate that the theory may be at worst performance for media with narrow pore size distributions. Therefore, it can be concluded that the theory proved to be quite inapplicable to these data and that the air-entry effect on the main branch drainage curves was strongly connected to the failure of the independent domain theory, although it was not the sole origin of the discrepancies.

Topp (50) has used a uniformly packed column of sandy loam soil to a controlled series of wetting and drying changes. From the poor agreement between the predictions and the experimental data it is evident that the independent domain model is not adequate for this sandy loam soil for pressure heads ranging from 0 to -280 cm of water. The nature of the discrepancy between the experiment and the prediction is quite similar to that shown by Topp and Miller (52) for the monodispersed glass-bead sample.

Poulouvassilis (44) has used granular porous bodies to assess hysteresis behavior and to compare them with the predictions of the independent domain concept. The results showed that the predictions were in very good agreement with the experimental data.

To modify the inadequacies of the independent domain theory of hysteresis Topp (51) introduced an extra extension to the theory by including two types of pore interactions. In the independent domain theory only the shapes of the pores determine the draining and filling characteristics of each pore, but in the introduced extension the draining and filling of each pore was assumed to depend on the state of neighboring pores as well as the pore geometry. The ratios of changes in water content of the soil during drying and rewetting over a given pressure head range has been used to determine the importance of pore interactions and to separate the two types of pore blockage. Primary scanning curve data for porous materials ranging from glass beads to clay loam soil has shown that pore blockage against air-entry during the drying of a soil near saturation and pore blockage against water-entry during rewetting of a relatively dry soil were the two major types of pore interactions. The predictions based on the introduced extension are considerable improvements over predictions by the independent domain theory. Although, this extension to the domain theory has improved the model, it has complications when applied in practice.

By considering a different integration domain for the distribution function $f(\psi_d, \psi_w)$, Mualem (29) derives *Model II*. Using the theory developed by Mualem (29), the following expressions for the moisture content can be derived:

- (1) For an uneven order drying scanning curve of order n :

$$\theta_{nd}(\psi) = \theta_w(\psi) + (\theta_w(\psi_n) - \theta_w(\psi)) \left[\frac{\theta_d(\psi) - \theta_w(\psi)}{\theta_s - \theta_w(\psi)} \right] + \sum_{i=1}^{i=n-1/2} \left[\frac{(\theta_w(\psi_{2i-1}) - \theta_w(\psi_{2i+1}))(\theta_d(\psi_{2i}) - \theta_w(\psi_{2i}))}{(\theta_s - \theta_w(\psi_{2i}))} \right] \quad (1)$$

- (2) For an even order wetting scanning curve of order n :

$$\begin{aligned} \theta_{mw}(\psi) = & \theta_w(\psi) + (\theta_w(\psi_{n-1}) - \theta_w(\psi)) \left[\frac{\theta_d(\psi_n) - \theta_w(\psi_n)}{\theta_s - \theta_w(\psi_n)} \right] \\ & + \sum_{i=2}^{i=n/2} \left[\frac{(\theta_w(\psi_{2i-3}) - \theta_w(\psi_{2i-1}))(\theta_d(\psi_n) - \theta_w(\psi_n))}{(\theta_s - \theta_w(\psi_n))} \right] \end{aligned} \quad (2)$$

(3) For an uneven order wetting scanning curve of order n :

$$\begin{aligned} \theta_{mw}(\psi) = & \theta_w(\psi) + (\theta_s - \theta_w(\psi)) \left[\frac{\theta_d(\psi_1) - \theta_w(\psi_1)}{\theta_s - \theta_w(\psi_1)} \right] \\ & + \sum_{i=1}^{i=n-1/2} (\theta_w(\psi_{2i}) - \theta_w(\psi)) \left[\frac{(\theta_d(\psi_{2i+1}) - \theta_w(\psi_{2i+1}))}{(\theta_s - \theta_w(\psi_{2i+1}))} - \frac{(\theta_d(\psi_{2i-1}) - \theta_w(\psi_{2i-1}))}{(\theta_s - \theta_w(\psi_{2i-1}))} \right] \end{aligned} \quad (3)$$

(4) For an even order drying scanning curve of order n :

$$\begin{aligned} \theta_{nd}(\psi) = & \theta_w(\psi) + (\theta_s - \theta_w(\psi_2)) \left[\frac{\theta_d(\psi_1) - \theta_w(\psi_s)}{\theta_s - \theta_w(\psi_1)} \right] + (\theta_w(\psi_n) - \theta_w(\psi)) \cdot \\ & \left[\frac{\theta_d(\psi) - \theta_w(\psi)}{\theta_s - \theta_w(\psi)} \right] + \sum_{i=2}^{i=n/2} (\theta_w(\psi_{2i-2}) - \theta_w(\psi_{2i})) \left[\frac{(\theta_d(\psi_{2i-1}) - \theta_w(\psi_{2i-1}))}{(\theta_s - \theta_w(\psi_{2i-1}))} \right] \end{aligned} \quad (4)$$

where $\theta_w(\psi)$, is volumetric moisture content on the main wetting curve for a pressure head ψ ; $\theta_d(\psi)$, is volumetric moisture content on the main drying curve for a pressure head ψ ; $\theta_{mw}(\psi)$, is volumetric moisture content on the wetting curve of order n for a pressure head ψ ; $\theta_{nd}(\psi)$, is volumetric moisture content on the drying curve of order n for a pressure head ψ ; θ_s , is saturated moisture content and ψ_i is the water potential at which the i -th reversal from wetting to drying (or drying to wetting) occurred.

The scanning curves predicted by the introduced model were in satisfactory agreement with the measured ones. Great improvement was achieved for the case in which the prediction based on usual *Everett* model (11) was poor. Since the introduced model was based on a modified independent domain theory, there are some limitations that are not circumvented, such as the large deviation of the predicted curves from the measured ones for cases in which appreciable hysteresis exists for ψ greater than the air-entry value.

Mualem's *Model II* was a 2-branch model. If the two main curves are given (θ_w, θ_d), all the other curves could be calculated. In the universal variant of this model (30) the two distribution functions were assumed equal:

$$f(\psi_d, \psi_w) = m(\psi_d) m(\psi_w) \quad (5)$$

In this case the required information for the determination of the distribution function $f(\psi_d, \psi_w)$ was reduced to one branch. The model is "universal" because it presents a "universal" relationship between the two main curves.

$$\theta(\psi) = [2\theta_s - \theta_w(\psi)] \cdot \frac{\theta_w(\psi)}{\theta_s} \quad (6)$$

Mualem (31) proved that when the water content is normalized between the minimum measured value (θ_{\min}) and the resaturation value (θ_s), the theoretical primary curves duplicate the main hysteresis curve. Based on this property of the universal model, a procedure was developed to predict the complete hysteresis domain when only the primary hysteresis curve is available. However, the universal model was not recommended for unrestricted use as a predictive tool of scanning curves. Good agreement between theory and observations was found for sand, which displays a zero air entry value. In other cases, the prediction errors at high saturations were quite large. A comprehensive examination of the universal model using data of 10 soils (31) indicated that the upper limit of the effective saturation (S_e) under which the model generally yields acceptable results varies significantly for different soils but with a characteristic trend. This limiting value of S_e diminishes as the granular fraction of the soil increases. That gave grounds for hypothesizing that poor performance of the universal model results from neglecting the effect of pore water blockage against air entry.

Dependent Domain Theory

The basis of the dependent domain theory is the following equation (9):

$$\theta = \iint P_d(\psi_w, \psi_d, \theta, \psi) \cdot (\psi_w, \psi_d, \theta, \psi) f(\psi_w, \psi_d) d\psi_w d\psi_d \quad (7)$$

where $f(\psi_w, \psi_d)$ is the distribution function corresponding to the independent domain behavior of the porous medium, P_d is a weight function ($P_d \leq 1$) which represents the ratio between the volume of actually drained pores and the volume which would have been drained if the pores were independent. Similarly, P_w is the weight function for a wetting process. Function P_d accounts for pore blockage against air entry, and P_w for pore blockage against water. If $P_d = P_w$, Eq. (7) becomes identical with the independent domain relationship.

A different attempt for defining a dependent domain model of hysteresis has been made by Poulouvassilis and Childs (45). They defined two kinds of pore elements: α elements, have independent ψ_w values but the values of ψ_d depend on the capillary head ${}_r\psi_w$, at which the process switches from wetting to drying, and β elements, with independent ψ_d but with ψ_w depending on ${}_r\psi_d$ at which transition from drying to wetting takes place. All the parameters are located off the line. The pore distribution function becomes in a way a function of four variables, $F(\psi_w, \psi_d, {}_r\psi_w, {}_r\psi_d)$. Although the authors suggest some simplifications which make possible the derivation of F from measured scanning curves, the amount of experimental data required in order to determine F is so large (sets of primary and secondary wetting and drying scanning curves) as to prohibit use of the method. However, the results showed that the predictions were in satisfactory agreement with the experimental data.

Mualem and Dagan (33) presented a simplified dependent domain model of hysteresis (*Model III*) which incorporates two fundamental ideas of Everett (9) and Topp (51) together and was simple enough to be applied to unsaturated flows. It was

found that the simplified model leads to better results than the models based on independent domain model theories for soils having a major portion of their hysteresis loop in the range of air entry value. However, the better performance of *Model III* was achieved at the expense of using more measured data (it requires a primary drying scanning curve in addition to the main hysteresis loop for calibration) and detraction from the simplicity of the model.

Mualem (31) modified the dependent domain theory. The modified model corrects the moisture content changes calculated on the basis of the independent domain ($\Delta\theta_0$) by multiplying these changes with a correction factor $P_d(\theta)$:

$$P_d(\theta) = \frac{\theta_s(\theta_s - \theta)}{(\theta_s - \theta_w(\psi^+))^2} \quad (8)$$

where ψ^+ is the potential for which $\theta_d(\psi^+) = \theta$. For a wetting curve of order n the correction factor is $P_d(\theta(\psi_n))$, ψ_n being the pressure head of the n -th reversal point. For a drying curve the factor is $P_d(\theta(\psi))$, where ψ is the current pressure head for which the moisture content is being calculated. This implies that for a drying curve P_d is to be calculated iteratively, hence the implicit character of the model. Computed primary and secondary scanning curves derived by this model showed good agreement with measured data. The results are compared with computed curves based on *Model II* of Mualem (29). The new model seems to agree with observation much better than *Model II*, which uses the same amount of data for calibration.

Parlange's model

Parlange (39) developed a conceptual model which requires knowledge of one boundary instead of two boundaries, as in Mualem's case (31). In this model Parlange (39) assumed that the distribution function is only the function of ψ_d :

$$f(\psi_d, \psi_w) = f(\psi_d) \quad (9)$$

Furthermore, Parlange (39) pointed out that in the determination of the moisture retention characteristics the actual wetting boundary curve is seldom obtained. This implies that only uneven order drying and even order wetting scanning curves can be measured.

To understand the principle of Parlange's model (39), consider a drying scanning curve starting at potential ψ_1 on the wetting boundary of the curve. Then:

$$\theta_d(\psi, \psi_1) = \theta_w(\psi) + \int_{\psi_1}^{\psi} d\psi_w \int_{\psi}^{\psi_M} f(\psi_d, \psi_w) d\psi_d \quad (10)$$

Which correspond to the domain of integration shown in Fig. 2, where $|\psi_M|$ is a reasonable maximum suction. If f is a function of ψ_d only, then:

$$\theta_w = \int_{\psi}^{\psi_M} d\psi_w \int_{\psi_w}^{\psi_M} f(\psi_d) d\psi_d \quad (11)$$

and

$$\theta_d(\psi, \psi_1) = \theta_w(\psi) - (\psi - \psi_1) \left(\frac{d\theta_w}{d\psi} \right)_{\psi} \quad (12)$$

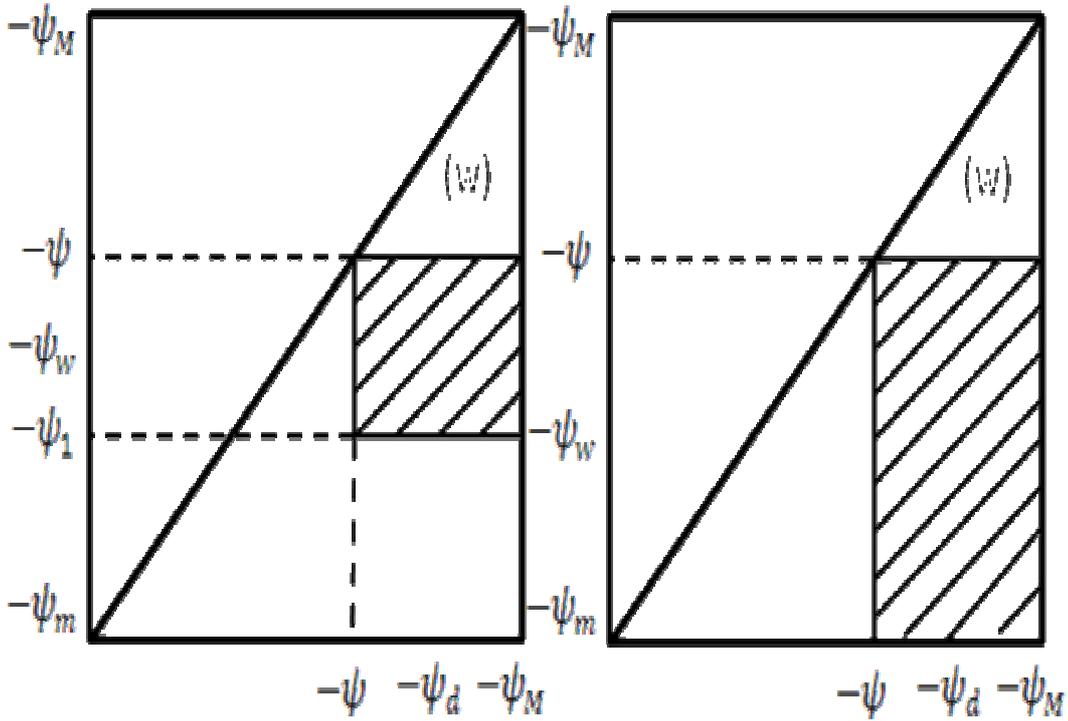


Fig. 2. Domains of integration for the function f in Eq. (11) and (14), as given by crosshatched rectangles for the drying (left) and wetting (right) scanning curves. The triangle (w) is the domain of integration of f defining θ_w in Eq. (12). If an opening becomes empty during the drying process (left), i.e., for $-\psi_1 < -\psi_d < -\psi$, then the attached pore is also emptied, since the openings are smaller than the pores. If the suction decreases during wetting (right), all corresponding pores are filled, since their smaller openings are automatically filled; in addition, pores of any size that have openings so small that the latter were never dried, i.e., for $-\psi_d > -\psi_2$, remain filled

Similarly, a wetting scanning curve starting at potential ψ_2 on the drying boundary of the loop is given by:

$$\theta_w(\psi, \psi_2) = \theta_w(\psi) + \int_{\psi_m}^{\psi} d\psi_w \int_{\psi_2}^{\psi_M} f(\psi_d, \psi_w) d\psi_d \quad (13)$$

which corresponds to the domain of integration shown in Fig. 1, where $|\psi_M|$ is a reasonable minimum suction, normally close to zero, or when f is a function of ψ_d only,

$$\theta_w(\psi, \psi_2) = \theta_w(\psi) - (\psi - \psi_m) \left(\frac{d\theta_w}{d\psi} \right)_{\psi_2} \quad (14)$$

If the drying boundary is given by (13) with $\psi_1 = \psi_m$, then $\theta_w(\psi, \psi_2)$ in (14) together with the boundary condition $\theta_w(\psi_2, \psi_2) = \theta_d(\psi_2, \psi_m)$ can be used in (12) instead of $\theta_w(\psi)$. This result is easily verified by direct substitution.

Comparison with experiments has showed that if the shape of the drying scanning curves varies smoothly, then the drying boundary of the loop was indeed

sufficient to predict all scanning curves. However, if the shape of the drying scanning curves changed abruptly, the model was applicable. However, the drying boundary yields only the wetting scanning curves, and the wetting boundary yields only the drying scanning curves.

Nonetheless, application of the theory is mathematically not trivial (34). Using a modified Brooks and Corey equation (4), Hogarth et al. (20) express the main wetting curve as:

$$\begin{aligned} \theta_w(\psi) &= \theta_{ae} \left(\frac{\psi_{ae}}{\psi} \right)^\lambda && \text{for } |\psi| > |\psi_{ae}| \\ \theta_w(\psi) &= \theta_{ae} \left(1 + \lambda - \lambda \frac{\psi_{ae}}{\psi} \right) && \text{for } |\psi_{we}| < |\psi| \leq |\psi_{ae}| \end{aligned} \quad (15)$$

and

$$\theta_w(\psi) = \theta_s \quad \text{for } |\psi| < |\psi_{we}| \quad (16)$$

where ψ_{ae} is air entry potential; ψ_{we} is water entry potential; λ is a dimensionless shape factor; θ_s is the saturated moisture content; and θ_{ae} is the moisture content on the main wetting curve at the air entry potential, which is calculated as:

$$\theta_{ae} = \frac{\theta_s}{1 + \lambda - \lambda \left(\frac{\psi_{we}}{\psi_{ae}} \right)} \quad (17)$$

The main drying curve can be calculated according to the expression:

$$\begin{aligned} \theta_d(\psi) &= \theta_{ae} \left(\frac{\psi_{ae}}{\psi} \right)^\lambda \left(1 + \lambda - \lambda \frac{\psi_{we}}{\psi} \right) && \text{for } |\psi| > |\psi_{ae}| \\ \theta_d(\psi) &= \theta_s && \text{for } |\psi| \leq |\psi_{ae}| \end{aligned} \quad (18)$$

The Parlange hysteresis model (39), which was initially formulated using the Brooks and Corey equation (4), was modified to use the well known van Genuchten (53) equation to describe the WRC (3). This model uses a simplified expression of van Genuchten equation by taking $\theta_r = 0$ (even if the residual volumetric water content can have an important role as a curve fitting parameter). In the following, θ stands for $(\theta - \theta_r)$, then $\theta(\psi) \rightarrow 0$ as $\psi \rightarrow 0$. The van Genuchten (53) model becomes:

$$\theta_{vG} = \theta_s \left[\frac{1}{1 + (\alpha\psi)^n} \right]^m \quad (19)$$

where θ_{vG} is volumetric moisture content estimated by the van Genuchten equation (53) and m , n and α correspond to fitted parameters of the equation. The authors defined a parameter $C(\psi)$ as the specific capacity:

$$C(\psi) = \theta_s m n \alpha (\alpha\psi)^{n-1} \left[\frac{1}{1 + (\alpha\psi)^n} \right]^{m+1} \quad (20)$$

Using the van Genuchten equation (53) to fit data of the main wetting curve, the main drying curve can be expressed as:

$$\theta_d = \theta_{vG}(\psi) + (\psi - \psi_d)C(\psi) \quad (21)$$

where θ_d is the calculated (predicted) volumetric water content on the main drying curve and ψ_d is the water pressure at the inversion point from wetting to drying. Braddock et al. (3) have also presented other equations that allow predicting primary and secondary hysteresis curves.

EMPIRICAL MODELS

Empirical models are based on an analysis of WRC shape and properties. These models use close-formed empirical expressions to represent hysteresis curves. They are often developed for a specific soil and they do not claim general validity because their derivation is not based on a physical representation of hysteresis. Among these models, one can identify: a) the interpolation model developed by Pickens and Gilham (42), Hoa et al. (19) and Dane and Wierenga (5); b) the linear model developed by Hanks et al. (15); c) the slope model developed by Jaynes (21) derived from Dane and Wierenga's (5) work and d) the scaling-down model developed by Scott et al. (48).

Interpolation model

The interpolation model calculates the value of θ of the new soil – water pressure from the θ -values of the main wetting and drying curves, θ_w and θ_d .

$$C = (\theta^{n+1} - \theta^n) / (P^{n+1} - P^n) \quad (22)$$

where C is the differential or specific water capacity, θ is the volumetric water content and the subscripts identify the values at the new time ($n+1$) and the old time (n) used in the numerical scheme. For wetting process:

$$\theta^{n+1} = c_1 \theta_d(P^{n+1}) + (1 - c_1) \theta_w(P^{n+1}) \quad (23)$$

where

$$c_1 = \left[\frac{\alpha_1}{P^{n+1} - P_{tr} + \alpha_1} \right] w_1 \quad (24)$$

$$w_1 = [\theta(P_{tr}) - \theta_w(P_{tr})] / [\theta_d(P_{tr}) - \theta_w(P_{tr})] \quad (25)$$

For drying, θ^{n+1} is found from:

$$\theta^{n+1} = c_2 \theta_w(P^{n+1}) + (1 - c_2) \theta_d(P^{n+1}) \quad (26)$$

where

$$c_2 = \left[\frac{\alpha_2}{P_{tr} - P^{n+1} + \alpha_2} \right] w_2 \quad (27)$$

$$w_2 = [\theta_d(P_{tr}) - \theta(P_{tr})] / [\theta_d(P_{tr}) - \theta_w(P_{tr})] \quad (28)$$

where P_{tr} is the transition pressure, the pressure at which the soil changes from wetting to drying or drying to wetting, w_1 and w_2 are weighting factors which are dependent on the water contents at the transition pressure and are required for secondary or higher scanning curves, α_1 and α_2 determine the rate of the scanning curve for a wetting and drying process, respectively. It should be noted that the values of 1.8 and 1.2 have been suggested for α_1 and α_2 , respectively by Hanks et al. (15). However, the α -values can be calculated from information contained in the main wetting and drying curves. Therefore:

$$\begin{aligned} \alpha_1 &= \exp[4 + P_{tr} / (P_e - P_c)] \\ \alpha_2 &= P_s - P_{tr} \end{aligned} \quad (29)$$

where P_e is the air-entry soil-water pressure head, P_c is the pressure where the hysteresis curves merge, and P_s is the pressure at which the main curves separate.

Linear model

The linear model approximates the scanning curves by a straight line spanning the main wetting and drying curves. In this model, the slope of the line is arbitrary with the only constraint that it be less than the slope of the main curves at intersection. For this *2-branch* model the equations are:

$$\theta_{1d}(\psi) = \theta_w(\psi_1) - \left[\frac{\theta_w(\psi_2) - \theta_d(\psi_1 - \alpha_1 \alpha_3)}{\alpha_1 \alpha_3} \right] |\psi - \psi_1| \quad (30)$$

for a primary drying scanning curve and

$$\theta_{1w}(\psi) = \theta_d(\psi_1) - \left[\frac{\theta_w(\psi_2 + \alpha_2 \alpha_3) - \theta_d(\psi)}{\alpha_2 \alpha_3} \right] |\psi - \psi_1| \quad (31)$$

for a primary wetting scanning curve.

where α_3 is the maximum pressure difference between the main wetting and drying curves at the same water content.

Slope model

The slope model is a modification of the interpolation method (5). In this model, C is calculated from the slopes of the main wetting and drying curves rather than from the water contents as in the interpolation method. For wetting curves:

$$C = w_3 \left(\frac{d\theta_w}{dP} \right) \quad (32)$$

with

$$w_3 = [\theta_d(P^{n+1}) - \theta(P^{n+1})] / [\theta_d(P^{n+1}) - \theta_w(P^{n+1})] \quad (33)$$

For drying, C is calculated in a similar way.

$$C = w_4 \left(\frac{d\theta_d}{dP} \right) \quad (34)$$

with

$$w_4 = [\theta(P^{n+1}) - \theta_w(P^{n+1})] / [\theta_d(P^{n+1}) - \theta_w(P^{n+1})] \quad (35)$$

where P is the soil water pressure head. An additional condition was placed on C for drying curves where $P \geq 1.5P_e$ (P_e is the air – entry soil – water pressure head). For these conditions, C was taken to be the maximum of either the value calculated in Equation 34 or the value calculated from a weighted average of the main curve slopes:

$$C = \frac{d\theta_d}{dP} + \alpha_4 \frac{d\theta_w}{dP} \quad (36)$$

where

$$\alpha_4 = [\theta_s - \theta(P^{n+1})] / 0.1\theta_s \quad (37)$$

and the maximum value allowed for α_4 was 1. Equation 36 was used to give C a non-zero value for scanning curves where $P^{n+1} > P_e$ rather than zero, as would be calculated by Equation (34) alone.

Scaling – down model

In this model the drainage scanning curves are predicted by rescaling the main drying curve to pass through the residual moisture content (θ_r) and the last reversal point from wetting to drying ($\theta_\Delta \psi_\Delta$) by replacing the saturated moisture content, θ_s , by:

$$\theta_s^* = \frac{\theta_\Delta(\theta_s - \theta_r) - \theta_r(\theta_s - \theta_d(\psi_\Delta))}{(\theta_d(\psi_\Delta) - \theta_r)} \quad (38)$$

Wetting scanning curves are predicted by replacing θ_r by:

$$\theta_r^* = \frac{\theta_\Delta(\theta_s - \theta_r) - \theta_s(\theta_w(\psi_\Delta) - \theta_r)}{(\theta_s - \theta_w(\psi_\Delta))} \quad (39)$$

All notations have been specified before. By doing this, the curve is forced through the last drying to wetting reversal point and θ_s .

It should be mentioned that other models were recently developed using different concepts. For example, the mathematical model developed by Preisach (46)

was applied to describe the hysteresis effects in the water retention curve by O’Kane et al. (37), using the concept of a continuous analog of a finite parallel connection of relays. The Haverkamp et al. (17) model, based on geometric scaling, was recently modified and simplified (12). Another hysteresis empirical model was developed for sandy soils using the basic concept of shape similarity between the WRC and the cumulative particle-size distribution function (16). In this case, the hysteresis is predicted from the basic properties of the soil, not from a WRC.

Summary and Comparison of models

Two main group of hysteresis models were reviewed in connection to their theories. These models were categorized into *conceptual* and *empirical* models. The first group is based on the domain theory of capillary hysteresis and the second group relies on the analysis of observed WRC shape and properties. *Conceptual* models included the *independent and dependent domain theories* and *Parlange's model*, while *empirical* models consisted of the *interpolation; linear; Slope and Scaling – down* models. Several authors have compared these different models. Viaene et al. (54), following a statistical analysis of hysteresis models, concluded that the best 2 branch models were conceptual models (Mualem II and IV), while the Parlange model was selected as the best choice for hysteresis prediction using a single branch. The same conclusion was reached by Si and Kachanoski (49) about one branch models. However, Jaynes' comparison (21 and 22) led to the conclusion that none of the methods were consistently better than the others, even for the more complex models with more than two branches. Jaynes also concluded that the linear model (empirical type of model) appears to be the best approach to predict hysteresis. Maqsoud et al. (27) indicated that the Universal Mualem model did not predict the WRC adequately. However, the two versions of the Parlange model (22 and 3) allow for good predictions of the main drying curves. More recently, different studies (3 and 17) suggested that the Parlange model, that uses the concept of rational extrapolation, was the best model to predict hysteresis of the WRC. Braddock et al. (3) proposed a new formulation of the Parlange model using the Van Genuchten (53) equation instead of Brooks and Corey’s (4). However, this version of the Parlange model should be examined in most texture soils.

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هیستریسیس؛ پدیده و مدل سازی در روابط آب و خاک

عزیزاله ایزدی^{۱*}، بیژن قهرمان^{۱**} و کامران داوری^{۱*}

^۱ بخش مهندسی آب، دانشکده کشاورزی، دانشگاه فردوسی مشهد، مشهد، جمهوری اسلامی ایران
چکیده - هیستریسیس در روابط مربوط به آب و خاک یک پدیده کاملاً شناخته شده می باشد. در این مقاله، پدیده هیستریسیس از دیدگاه مدل های مربوط به آن مورد مطالعه قرار گرفته است. تاکنون، مدل های مختلفی برای توصیف هیستریسیس در منحنی رطوبتی ارائه شده است که شامل دو گروه اصلی مدل های مفهومی و مدل های تجربی می باشد. گروه اول بر مبنای تئوری هیستریسیس مؤئینه ای و گروه دوم بر مبنای تحلیل شکل و خصوصیات منحنی رطوبتی اندازه گیری شده می باشد. مدل های مفهومی شامل تئوری حوزه مستقل، تئوری حوزه وابسته و مدل پارلانژ و مدل های تجربی شامل مدل های درون یابی، خطی، شیب و کوچک نمودن مقیاس[†] می باشد. نتایج مطالعات محققین مختلف نشان می دهد که مدل پارلانژ که از مفهوم برون یابی منطقی استفاده می کند بهترین مدل برای پیش بینی هیستریسیس در منحنی رطوبتی می باشد.

واژه های کلیدی: مدل مفهومی، مدل تجربی، مدل پارلانژ، هیستریسیس

† Scaling-down

* به ترتیب دانشجوی دکتری، استاد و دانشیار
** مکاتبه کننده